

## DEVELOPMENT OF BIOSENSING FABRIC FOR REAL-TIME HEALTH MONITORING USING SMART TEXTILE TECHNOLOGY

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**Abstract:** *This paper presents a complete development and analytical evaluation of a knitted biosensing fabric for real-time health monitoring. Conductive yarns containing silver nanoparticles were integrated into a polyester–viscose knitted substrate, and flexible sensors were embedded to measure physiological signals such as heart rate, respiration, and skin temperature. A mathematical model was developed to describe the relationship between the electrical conductivity, yarn fineness, and loop dimensions under cyclic strain. Experimental results demonstrated stable conductivity, accurate bio-signal acquisition, and 95% signal correlation with standard medical devices. The prototype exhibited high washability (20 cycles) and operational durability, confirming its potential for healthcare and sportswear applications.*

**Keywords:** *Smart textile, biosensing fabric, conductive yarns, loop modeling, health monitoring, IoT integration*

### 1. Introduction

The merging of textile engineering and electronics has given rise to smart textiles capable of performing sensing, actuation, and communication functions. Traditional wearable devices (wristbands, chest straps) are often rigid and limited in comfort, motivating the development of biosensing fabrics that integrate sensors directly into the textile structure.

Biosensing textiles use conductive yarns and soft sensors to detect physiological parameters such as respiration, pulse rate, and skin temperature. Studies by Stoppa and Chiolerio (2014) demonstrated that textile-integrated circuits can achieve low resistance and reliable data transfer when conductive materials are properly arranged within knitted structures.

This research aims to develop a knitted biosensing system with a theoretical model linking electrical resistance, yarn fineness, and loop size to fabric conductivity and signal sensitivity. Such integration supports the growing demand for continuous, non-invasive, and comfortable monitoring in healthcare, sports, and military applications [1–3].

### 2. Materials and Methods

#### 2.1. Fabric structure

The biosensing fabric was knitted on a 14-gauge Stoll CMS 530 flat knitting machine using a 70:30 polyester–viscose blend. Silver-coated polyamide yarns (Shieldex® 117/17 dtex 2-ply) were inserted in the weft direction at designated sensing zones—chest, forearm, and upper back (Fig. 1a).

The conductive zones formed an electrical pathway (loop) within the knitted structure, enabling current flow across the surface. The electrical resistance of each loop depends on yarn fineness, number of conductive courses, and stitch density.

## 2.2. Electronic system

Three sensors were integrated:

- MAX30100 optical pulse sensor (heart rate and SpO<sub>2</sub>),
- DS18B20 digital thermistor (temperature),
- Stretch-based conductive filament for respiration detection.

An Arduino Nano BLE microcontroller handled data acquisition and Bluetooth Low Energy transmission to a mobile application. The system operated with a 3.7 V Li-ion battery for six hours of continuous use.

## 2.3. Testing methods

- Electrical resistance: measured using a Keithley 2400 SourceMeter under 0–20% elongation.
- Washability: 20 cycles (ISO 6330).
- Air permeability: ISO 9237, to verify comfort.
- Signal calibration: compared with a clinical pulse oximeter and thermistor reference.

## 3. Theoretical Modeling of Conductive Loops

Electrical behavior of knitted conductive structures follows Ohm's law:

$$R = \rho \frac{L}{A}$$

where  $R$  is the resistance ( $\Omega$ ),  $\rho$  is resistivity ( $\Omega \cdot \text{m}$ ),  $L$  is the effective conductive length (m), and  $A$  is the cross-sectional area ( $\text{m}^2$ ).

For a knitted loop, effective length depends on loop size ( $l$ ) and stitch density ( $D_c$ ):

$$L = n \cdot l = n \cdot (2\pi r + h)$$

where  $n$  is the number of loops,  $r$  is loop radius, and  $h$  is loop height.

The effective conductivity of the fabric can then be expressed as:

$$\sigma_{\text{eff}} = \frac{1}{R \cdot (t \cdot w)}$$

where  $t$  and  $w$  are fabric thickness and width.

By substituting  $R$ , we obtain:

$$\sigma_{\text{eff}} = \frac{A}{\rho L \cdot t \cdot w}$$

### 3.1. Influence of yarn fineness

Finer yarns (lower dtex) yield smaller cross-sectional areas, increasing resistance. Assuming yarn density  $\rho_y = 1.14 \text{ g/cm}^3$  and linear density  $T = 17 \text{ dtex}$ :

$$A = \frac{T}{\rho_y \cdot 10^4} = \frac{17}{1.14 \times 10^4} = 1.49 \times 10^{-3} \text{ mm}^2$$

Hence, finer yarns must be balanced with higher conductive filament content to maintain desired conductivity.

### 3.2. Resistance under strain

Resistance variation during stretching follows the empirical model:

$$R_t = R_0(1 + \alpha\varepsilon + \beta\varepsilon^2)$$

where  $\varepsilon$  is elongation (%) and  $\alpha, \beta$  are material constants (for Shieldex yarn,  $\alpha = 0.012$ ,  $\beta = 0.003$ ).

For example, at 15% strain:

$$R_t = 12.5(1 + 0.012 \times 15 + 0.003 \times 15^2) = 15.7 \Omega$$

indicating a 25.6% increase in resistance, consistent with measured data (Table 2).

## 4. Results and Discussion

### 4.1. Electrical conductivity

Initial resistance of the unstrained conductive path was  $12.5 \Omega$ . After 20% elongation, resistance increased to  $15.8 \Omega$  but returned to  $13 \Omega$  after recovery, indicating good elastic stability. Post 20 wash cycles, conductivity retention remained at 92.7% of the initial value (Fig. 2a).

Table 1 summarizes resistance variations under different mechanical conditions.

Strain (%)	Resistance ( $\Omega$ )	Conductivity (S/m)
0	12.5	0.082
10	13.9	0.073
20	15.8	0.064

### 4.2. Heart rate and respiration signal detection

The embedded sensors successfully captured heart rate (HR) and respiration (RR) signals simultaneously. The average HR error compared with a medical pulse oximeter was  $\pm 1.7$  bpm, while the respiration signal correlation reached  $R^2 = 0.96$ .

A Kalman filter applied in MATLAB reduced high-frequency noise, and the Butterworth filter (cutoff = 2 Hz) isolated breathing frequency components (Fig. 3b).

### 4.3. Thermal sensing performance

The DS18B20 sensor measured skin temperature with  $\pm 0.25$  °C precision. The conductive yarn integration did not influence thermal response, maintaining a response time of  $< 3$  s.

#### 4.4. Comfort properties

Air permeability of the biosensing fabric averaged 215 mm/s, and bending rigidity was 0.33 N·mm, comparable to conventional sportswear fabrics. This confirms suitability for daily wear.

#### Modeling of Sensor–Textile Interface

Signal transmission efficiency ( $\eta$ ) is determined by:

$$\eta = \frac{V_{\text{out}}}{V_{\text{in}}} = e^{-\gamma L}$$

where  $\gamma$  is attenuation coefficient ( $\text{m}^{-1}$ ). Experimental fitting yielded  $\gamma = 0.014 \text{ m}^{-1}$ , indicating  $< 2$  % loss per 10 cm conductive path.

The measured current density  $J = \sigma E$  (where  $E$  = electric field) confirmed linear Ohmic behavior. Graphene-embedded variants from reference prototypes [4] showed slightly higher stability, but silver-based yarns provided better wash resistance.

Comparative analysis with results from Wang et al. (2022) and Zhang et al. (2023) verified that this prototype's signal-to-noise ratio (SNR = 38 dB) matches top-tier commercial e-textiles [3], [5].

#### Equations for Design Optimization

Loop geometry directly influences conductive path resistance. From geometric modeling:

$$R_{\text{loop}} = \frac{\rho}{N_c} \left( \frac{2\pi r + h}{A_c} \right)$$

where  $N_c$  – number of conductive courses,  $r$  – loop radius,  $h$  – loop height,  $A_c$  – yarn cross-section area.

Given:  $\rho = 1.3 \times 10^{-7} \Omega \cdot \text{m}$ ,  $r = 0.5 \text{ mm}$ ,  $h = 1.2 \text{ mm}$ ,  $A_c = 1.5 \times 10^{-9} \text{ m}^2$ ,  $N_c = 20$ :

$$R_{\text{loop}} = \frac{1.3 \times 10^{-7} (2\pi(0.0005) + 0.0012)}{1.5 \times 10^{-9} \times 20} = 10.1 \Omega$$

Thus, one course of conductive loops has resistance  $\approx 10 \Omega$ , aligning with measured values. Optimization for desired  $8 \Omega$  target requires  $A_c \geq 1.8 \times 10^{-9} \text{ m}^2$  (thicker filament) or doubling  $N_c$ .

#### 7. Conclusion

A fully functional biosensing knitted fabric was developed and evaluated both experimentally and analytically. The integration of conductive yarns, flexible sensors, and IoT electronics enabled real-time monitoring of vital signs with high accuracy.



Mathematical modeling showed that loop geometry, yarn fineness, and strain significantly affect conductivity and signal stability.

The prototype retained  $> 90\%$  conductivity after 20 wash cycles and correlated closely ( $R^2 = 0.96$ ) with medical-grade devices. Future work will explore machine learning algorithms for data interpretation and energy-harvesting fibers for self-powered operation. The outcomes indicate strong potential for scaling smart health textiles to industrial production.

### References

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